Analytic Left Inversion of SISO Lotka-Volterra Models[†]

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Overview

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- 2. Preliminaries on Fliess Operators and Their Inverses
- **3.** Left System Inversion of Lotka-Volterra Input-Output Systems
- **4.** Numerical Simulations
- **5.** Conclusions



1. Introduction

- Given an operator F, describing the dynamics of a system, and a function y in its range, the left inversion problem (LIP) is to determine a unique input u such that y = F[u].
- A sufficient condition (but not necessary) for solving this problem in a state space setting is to have well defined relative degree (Isidori, 1995).
- The solution of LIP does not require a state space realization.
- Fliess operators provide an explicit analytical solution.
- Introduced by M. Fliess in 1983, Fliess operators are analytic input-output systems described by coefficients and iterated integrals of the inputs.
- Fliess operators can be viewed as a functional generalization of a Taylor series. For example, any Volterra operator with analytic kernels has a Fliess operator representation.



2. Preliminaries

Population models:

• Here we apply the method to the population dynamical system:

$$\dot{z}_i = \beta_i z_i + \sum_{j=1}^n \alpha_{ij} z_i z_j, \quad i = 1, 2, \dots, n,$$
 (Lotka-Volterra model)

where $z_i \propto to$ the *i*-th population, β_i is the growth rate for the *i*-th population, and α_{ij} weights the effect of the *j*-th species on the *i*-th species.

- Input-output models are obtained by introducing time dependence on the $\beta_i(t)$'s or $\alpha_{ij}(t)$'s (inputs), and assuming y = h(z) (outputs).
- For n = 2,

$$\begin{pmatrix} \dot{z}_1 \\ \dot{z}_2 \end{pmatrix} = \begin{pmatrix} \beta_1 z_1 - \alpha_{12} z_1 z_2 \\ -\beta_2 z_2 + \alpha_{21} z_1 z_2 \end{pmatrix}$$
(Predator-Prey model)

The vector fields are complete within the first quadrant giving concentric periodic trajectories about $z_e = (\beta_2/\alpha_{21}, \beta_1/\alpha_{12})$.



Fliess Operators:

- Let $X = \{x_0, x_1, \dots, x_m\}$ be an alphabet and X^* the set of all words over X (including the empty word \emptyset).
- A formal power series is any mapping $c: X^* \to \mathbb{R}^{\ell}$. Typically, c is written as a formal sum $c = \sum_{\eta \in X^*} (c, \eta) \eta$, and the set of all such series is $\mathbb{R}^{\ell} \langle \langle X \rangle \rangle$.
- For a measurable function $u : [a, b] \to \mathbb{R}^m$ with finite L_1 -norm, define $E_\eta : L_1^m[t_0, t_0 + T] \to \mathcal{C}[t_0, t_0 + T]$ by $E_\emptyset[u] = 1$, and $E_{x_i\eta'}[u](t, t_0) = \int_{t_0}^t u_i(\tau) E_{\eta'}[u](\tau, t_0) d\tau,$

where $x_i \in X$, $\eta' \in X^*$ and $u_0 \triangleq 1$.

- Note that to each letter x_i has been assigned a function u_i .
- For each $c \in \mathbb{R}^{\ell} \langle \langle X \rangle \rangle \Rightarrow F_c[u](t) = \sum_{\eta \in X^*} (c, \eta) E_{\eta}[u](t, t_0)$, which is called a Fliess operator (Fliess, 1983).



Fliess Operator Inverses:



 $\Rightarrow F_c F_d = F_c \sqcup d, \text{ where } \sqcup \text{ denotes the shuffle product.}$

Fig. 2.1: Product connection.



Fig. 2.2: Cascade connection.



Fig. 2.3: Feedback connection.

 $\Rightarrow F_c \circ F_d = F_{c \circ d}, \text{ where } c \circ d \text{ denotes}$ the composition product of $c \in \mathbb{R}^{\ell} \langle \langle X \rangle \rangle$ and $d \in \mathbb{R}^m \langle \langle X \rangle \rangle$ (Gray et al., 2014)

Given $c, d \in \mathbb{R}^m \langle \langle X \rangle \rangle$, y satisfies

$$y = F_c[v] = F_c[u + F_d[y]].$$

If there exists e so that $y = F_e[u]$, then $F_e[u] = F_c[u + F_{d \circ e}[u]]$. (contraction!)



On the other hand, $v = u + F_{d \circ c}[v] \Rightarrow (I + F_{-d \circ c})[v] = u.$

Apply the compositional inverse to both sides of this equation:

$$v = (I + F_{-d \circ c})^{-1} [u] := (I + F_{(-d \circ c)^{\circ - 1}}) [u].$$

In which case, $F_{c@d}[u] = F_c[v] = F_{c\circ(\delta - d\circ c)^{\circ - 1}}[u]$, (explicit formula!) or equivalently, $c@d = c \circ (\delta - d \circ c)^{\circ - 1}$, where $F_{\delta} := I$.

The set of operators $\mathscr{F}_{\delta} = \{I + F_c : c \in \mathbb{R}\langle\langle X \rangle\rangle\}$, forms a group under composition, in particular, a Faà di Bruno Hopf algebra with antipode, α , satisfying

$$(\delta + c)^{\circ -1} := \delta + c^{\circ -1} = \delta + \sum_{\eta \in X^*} (\alpha \, a_\eta)(c) \, \eta,$$

where $c^{\circ -1}$ denotes the composition inverse of c and

$$a_{\eta} : \mathbb{R}\langle\langle X \rangle\rangle \to \mathbb{R} : c \mapsto (c, \eta).$$

Remark: The antipode has an explicit series representation (Gray & Duffaut Espinosa, 2011, 2014).



Now observe that any $c \in \mathbb{R}\langle\langle X \rangle\rangle$ can be written as $c = c_N + c_F$, where $c_N := \sum_{k>0} (c, x_0^k) x_0^k$ and $c_F := c - c_N$.

Definition 2.1: Given $c \in \mathbb{R}\langle\langle X \rangle\rangle$, let $r \geq 1$ be the largest integer such that $\operatorname{supp}(c_F) \subseteq x_0^{r-1}X^*$. Then c has relative degree r if the linear word $x_0^{r-1}x_1 \in \operatorname{supp}(c)$, otherwise it is not well defined.

Remark: This definition coincides with the usual definition of relative degree given in a state space setting. But this definition is **independent** of the state space setting.

Definition 2.2: Given $\xi \in X^*$, the corresponding left-shift operator is

$$\xi^{-1}: X^* \to \mathbb{R}\langle X \rangle : \eta \mapsto \begin{cases} \eta' & : \eta = \xi \eta' \\ 0 & : \text{ otherwise.} \end{cases}$$

Remark: The operation $F_c/F_d = F_{c/d}$ is given by $c/d := c \sqcup d^{\sqcup \sqcup -1}$, where $c^{\sqcup \sqcup -1} := (c, \emptyset)^{-1} \sum_{k=0}^{\infty} (c')^{\sqcup \sqcup k}$, and $c' = 1 - c/(c, \emptyset)$ is proper.



$$\begin{array}{l} y = F_{c}[u] \\ y^{(1)} = F_{x_{0}^{-1}(c)}[u] \\ \vdots \\ y^{(r-1)} = F_{(x_{0}^{r-1})^{-1}(c)}[u] \\ y^{(r)} = F_{(x_{0}^{r})^{-1}(c)}[u] \\ + u F_{(x_{0}^{r-1}x_{1})^{-1}(c)}[u]. \end{array} \right\} \quad u = \frac{v - F_{(x_{0}^{r})^{-1}(c)}[u]}{F_{(x_{0}^{r-1}x_{1})^{-1}(c)}[u]} \quad (y^{(r)} = v) \\ = \frac{-F_{(x_{0}^{r})^{-1}(c-c_{y})}[u]}{F_{(x_{0}^{r-1}x_{1})^{-1}(c)}[u]} = -F_{d}[u], \\ \left(d = \frac{(x_{0}^{r})^{-1}(c-c_{y})}{(x_{0}^{r-1}x_{1})^{-1}(c)}.\right) \end{aligned}$$

Theorem 2.3: Suppose $c \in \mathbb{R}\langle\langle X \rangle\rangle$ has relative degree r. Let y be analytic at t = 0 with generating series $c_y \in \mathbb{R}_{LC}[[X_0]]$ satisfying $(c_y, x_0^k) = (c, x_0^k), \ k = 0, \dots, r-1$. (Here $X_0 := \{x_0\}$.) Then the input

$$u(t) = \sum_{k=0}^{\infty} (c_u, x_0^k) \frac{t^k}{k!},$$

where $c_u = ((x_0^r)^{-1}(c - c_y)/(x_0^{r-1}x_1)^{-1}(c))^{\circ -1}$, is the unique solution to $F_c[u] = y$ on [0, T] for some T > 0.

Remark: The condition on c_y ensures that y is in the range of F_c .



3. Left System Inversion of LV Input-Output Systems

Four SISO predator-prey systems with output $y = z_1$ (prey):

I/0 map	state space realization	rel. degree
$F_c: \beta_1 \mapsto y$	$g_0(z) = \begin{bmatrix} -\alpha_{12}z_1z_2\\ -\beta_2z_2 + \alpha_{21}z_1z_2 \end{bmatrix}, \ g_1(z) = \begin{bmatrix} z_1\\ 0 \end{bmatrix}$	1
$F_c: \alpha_{12} \mapsto y$	$g_0(z) = \begin{bmatrix} \beta_1 z_1 \\ -\beta_2 z_2 + \alpha_{21} z_1 z_2 \end{bmatrix}, \ g_1(z) = \begin{bmatrix} -z_1 z_2 \\ 0 \end{bmatrix}$	1
$F_c: \beta_2 \mapsto y$	$g_0(z) = \begin{bmatrix} \beta_1 z_1 - \alpha_{12} z_1 z_2 \\ \alpha_{21} z_1 z_2 \end{bmatrix}, \ g_1(z) = \begin{bmatrix} 0 \\ -z_2 \end{bmatrix}$	2
$F_c: \alpha_{22} \mapsto y$	$g_0(z) = \begin{bmatrix} \beta_1 z_1 - \alpha_{12} z_1 z_2 \\ -\beta_2 z_2 \end{bmatrix}, \ g_1(z) = \begin{bmatrix} 0 \\ z_1 z_2 \end{bmatrix}$	2





The population system under study:

$$\begin{pmatrix} \dot{z}_1 \\ \dot{z}_2 \end{pmatrix} = \begin{pmatrix} -\alpha_{12}z_1z_2 \\ -\beta_2z_2 + \alpha_{21}z_1z_2 \end{pmatrix} + \begin{pmatrix} z_1 \\ 0 \end{pmatrix} u, \quad y = z_1$$

with $z_1(0) = z_{1,0}$ and $z_2(0) = z_{2,0}$. Make $\alpha_{12} = \alpha_{21} = \beta_2 = 1$.



Relative degree r = 1.





One must select an output function

$$y(t) = \sum_{k=0}^{\infty} (c_y, x_0^k) \frac{t^k}{k!},$$

where c_y is the generating series of y. It is sufficient to consider a polynomial of degree 3, so let $(c_y, \emptyset) = v_0$, $(c_y, x_0^i) = v_i$ for i = 1, 2, 3. Thus,

$$d := \frac{(x_0^r)^{-1}(c-c_y)}{(x_0^{r-1}x_1)^{-1}(c)} = -\alpha_{12}z_{2,0} - \frac{v_1}{z_{1,0}} + \left(\alpha_{12}\beta_2 z_{2,0} - \frac{v_2}{z_{1,0}}\right)$$
$$-\alpha_{12}\alpha_{21}z_{1,0}z_{2,0} - \frac{v_1\alpha_{12}z_{2,0}}{z_{1,0}}\right)x_0 + \frac{v_1}{z_{1,0}}x_1$$
$$+ \left(-\frac{v_1\alpha_{12}^2 z_{2,0}^2}{z_{1,0}} + \frac{v_1\alpha_{12}\beta_2 z_{2,0}}{z_{1,0}} - v_1\alpha_{12}\alpha_{21}z_{2,0}\right)$$
$$- \frac{2v_2\alpha_{12}z_{2,0}}{z_{1,0}} + \alpha_{12}^2\alpha_{21}z_{1,0}z_{2,0}^2 + 2\alpha_{12}\beta_2\alpha_{21}z_{1,0}z_{2,0}$$
$$- \frac{v_3}{z_{1,0}} - \alpha_{12}\beta_2^2 z_{2,0} - \alpha_{12}\alpha_{21}^2 z_{1,0}^2 z_{2,0}\right)x_0^2 + \cdots$$



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In which case,

$$c_{u} = (d^{\circ -1})_{N} = \frac{v_{1}}{z_{1,0}} + \alpha_{12}z_{2,0} + \left(\frac{v_{1}\left(-\frac{v_{1}}{z_{1,0}} - \alpha_{12}z_{2,0}\right)}{z_{1,0}} + \frac{v_{1}\alpha_{12}z_{2,0}}{z_{1,0}}\right) + \frac{v_{2}\alpha_{12}z_{2,0}}{z_{1,0}} + \frac{v_{2}$$

Design example:

Given

$$[t_1, t_2] = [12.5, 12.7] \quad (\Delta t = 0.2),$$

$$u(t_1) = 1, \ u(t_2) = 1.5,$$

▶ initial orbit exit point $[z_1(12.5), z_2(12.5)]^T = [3.82, 2.25]^T$,

►
$$y(t_2) = 2$$
,

find a smooth u(t) for $t \in (t_1, t_2)$ so that all constraints are satisfied.





Solution:

• Select the output as

$$y(t) = \sum_{k=0}^{\infty} (c_y, x_0^k) \frac{t^k}{k!} = v_1 t + v_3 t^3 / 3!.$$

- From Theorem 2.3, $c_u = (d^{\circ -1})_N$ is computed in terms of v_1 and v_3 .
- Solving

$$\begin{array}{c} c_y(v_1, v_3) \middle|_{\substack{x_0^k \to (0.2)^k/k!, k > 0 \\ c_u(v_1, v_3)}} \middle|_{\substack{x_0^k \to (0.2)^k/k!, k > 0 \\ x_0^k \to (0.2)^k/k!, k > 0}} = 1.5 \end{array} \right\} \leftarrow \begin{array}{c} \text{system of nonlinear} \\ \text{algebraic equations} \end{array}$$

gives the transfer input (up to order 6):

$$u(t) = -0.844733 - 3.22608(t - t_1) + 19.2847(t - t_1)^2 + 98.9718(t - t_1)^3 + 483.681(t - t_1)^4 + 1476.69(t - t_1)^5 + 2818.13(t - t_1)^6$$



4. Numerical Simulation

Note that $u(t_2) = 1.5$ and $y(t_2) = 2.0$, and the error is



Fig. 4.1: Prey (top) and predator (bottom) populations.







Fig. 4.2: Orbit transfer.



5. Conclusions and Future Work

- The LIP for SISO Lotka-Volterra systems was solved using Fliess operators having well defined relative degree.
- The method provides an exact, explicit and analytic formula for the LIP.
- The MIMO version of the Lotka-Volterra trajectory design problem is under review for the CDC 2015.
- Efficiency of the current software is currently being improved.